Research Article Pull-out Resistance Parallel to Grain of Threaded Steel Rod Glued-in Glubam with Edge Distance Variation

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Abstract: This study aimed to obtain the pull-out resistance parallel to the grain of the threaded steel rod glued-in glubam with various edge distances. The wood structures, both for connection and for reinforcement, used glued-in rods connection. However, there was no research on the application of glued-in-rod into the connection of structural elements from glued laminated bamboo (glubam) due to lack of information on the basic characteristics of the glued-in rod on laminated bamboo. This experiment tested the pull-out resistance and stiffness of the threaded steel rod bounded parallel to the grain in laminated bamboo with varying edge distances. The dimension of laminated bamboo specimens were100×100×100 mm, the threaded steel rod diameter was 10 mm, the drill hole diameter was 14 mm and this research used sikadur 732 as the adhesive. This experiment made eight various edge distances: 1d; 1.5d; 2d; 2.5d; 3d; 3.5d; 4d; and 4.5d, with d as the threaded steel rod diameter and made five replicas of each variation. The results showed that the 3d edge distance or greater had the constant pull-out resistance while less than 3d edge distance had less pull-out resistance. The slip modulus for the threaded steel rod glued-in glubam in this study was not influenced by edge distance with a range 3.732 kN/mm to 7.768 kN/mm.

Keywords: Edge distance, laminated bamboo, pull out resistance, slip modulus, threaded steel

INTRODUCTION

There are numerous researches on glued laminated bamboo (glubam) application for construction. The researches included beam and column structural elements (Xiao *et al.*, 2010; Sinha *et al.*, 2014; Karyadi and Susanto, 2017; Karyadi *et al.*, 2018).

Assembling structural elements into building structures require a connection using various shapes and materials. Recently, there was a development of a glued-in rod connector and its application in wood structure; both for connector (Gonzalez *et al.*, 2016; O'Neill *et al.*, 2017; Gattesco *et al.*, 2010) or reinforcement (Steiger *et al.*, 2015; Harte *et al.*, 2015).

However, there was no study in glued-in rod applications on the connection of laminated bamboo structural element. The reason were due to the lack of information on the base characteristic of glued-in rod in laminated bamboo. Research by Yan *et al.* (2016) offered information about the effect of the depth and diameter of the glued-in rod on the pull-out strength. Nonetheless, it left many unresearched parameters. Therefore, this research aimed to study the distance effect between the threaded steel rod and the edge of

laminated bamboo on the threaded steel rod pull-out resistance, slip modulus and types of failure.

Researchers have developed formulas to calculate the pull-out resistance of glued-in rod application in wood material. The formula developed by Steiger *et al.* (2006), Yeboah *et al.* (2013) and Yan *et al.* (2016) is usefull to calculate the glued-in rod pull-out resistance with edge distance greater than or equal to the allowed minimum distance. Generally, Stepinac *et al.* (2013) concluded that there are three main parameters involved in the above formula, e.g., the diameter of the glued-in rod, glued-in length and interfacial layer shear strength between wood and glue or between glue and rod. Similar to the conclusion above, Stepinac *et al.* (2013) and Yan *et al.* (2016) formulated the Eq. (1):

$$F = L_a \times \pi \times d_a \times f_v \tag{1}$$

With

F : Glued-in rod pull-out resistance

L_a : Glued-in length

- d_a : Diameter of the rod
- f_v : Interfacial shear strength
- π : Mathematical constant

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Fig. 1: Specimen; (a) Side view and (b) Cross section; e is the edge distance

Deng (1997) and New Zealand Timber Design Guide (NZW 14085 SC, 2007) developed another formula that including the distance between the gluedin rod and the edge of the timber displayed in the Eq. (2):

$$Q_{k} = Cd.k_{h}.k_{e}.k_{m}(l/d)^{0.86}.(d/20)^{1.62}.(h/d)^{0.5}.(e/d)^{0.5}$$
(2)

Within the Eq. (2); Q_k : pull-out resistance (N), (kN), k_b , k_e , k_m : bar type factor, epoxy factor, moisture factor respectively, 1: glued-in length (mm), d: diameter of steel rod (mm), h: diameter of the drill hole (mm), e: edge distance (mm), Cd = 8.54 for Deng (1997) formula and Cd = 6.73 for New Zealand Timber Design Guide (NZW 14085 SC, 2007).

The amount of slip during pull-out resistance were also crucial to note. This parameter is vital to determine the connection rigidity using the glued-in rod as stated in the slip modulus (K_s), calculated with the formula of (BS EN 26891, 1991):

$$K_s = \frac{0.4F_{\text{max}}}{\frac{4}{3}(d_{04} - d_{01})} \tag{3}$$

With,

MATERIALS AND METHODS

This research obtained 3-5 years old Asian bamboo (Dendrocalamus asper Backer) Malang, East Java, Indonesia. Then, cut and split them into 5×20 mm in cross-section and 1 m in length strips. Soaked the bamboo strips in a mixture solution of 1% boric acid (H₃BO₃) and 1% borax (Na₂B₄O₂) and dried. Glued the strips with less than 12% moisture content into each other using 268 g/m² urea-formaldehyde adhesive and cool-pressed in 2 MPa for four hours (Karyadi and Susanto, 2017). After, reaped the materials. Cut the



Fig. 2: Experimental setting up; (a) Testing configuration and (b) Photo of testing

laminated bamboo into 100 mm×100 mm×100 mm dimensions and drilled 14 mm diameter and 40 mm depth. The varying distances between the drill holes of the laminated bamboo edge were 1d, 1.5d, 2d, 2.5d, 3d, 3.5d, 4d, 4.5d; where d was the diameter of threaded steel rod with five replicas for each variation. The threaded steel rod with $f_y = 350$ MPa in 10 mm diameter and 250 mm length then put into drill holes. Before, gave the adhesive epoxy type in sikadur 732 brand (Fig. 1) in the drill hole.

This research used the Universal Testing Machine (UTM) with 1000 kN capacity and 0.1 kN precision to test the pull-out resistance and the dial gauge with 10 mm capacity and 0.01 mm precision to find the amount of the slip during the test. Figure 2 displays the test set up using loading configuration pull-compression.

This study used the Eq. (4) and (5) to calculate the amount of slip:

$$\Delta S = Y - \Delta L \tag{4}$$

Calculating ΔL used the formula:

$$\Delta L = \frac{P L_o}{\Delta S E} \tag{5}$$

Specimen code	Edge distance (e) (mm)	Diameter of treaded rod (d) (mm)	Anchored length (Lo) (mm)	Bounded area (A _s) (mm ²)
S1-d	10	10	40	1759
S1.5-d	15	10	40	1759
S2-d	20	10	40	1759
S2.5-d	25	10	40	1759
S3-d	30	10	40	1759
S3.5-d	35	10	40	1759
S4-d	40	10	40	1759
S4.5-d	45	10	40	1759
	Number of	Average of Pull-out	Standard	Average of shear
Specimen code	specimen	resistance (P) kN	deviation kN	strength (f _v) MPa
S1-d	5	13.020	0.835	7.401
S1.5-d	5	14.720	0.915	8.367
82-d	5	16.320	1.085	9.276
S2.5-d	4	17.400	0.483	9.890
83-d	5	19.720	1.190	11.209
S3.5-d	4	19.400	0.864	11.027
S4-d	4	18.700	0.600	10.629
S4.5-d	4	19,325	0,665	10,985



Table 1: Results for pull-out resistance test

Fig. 3: Relationship between pull-out resistance and edge distance

In Eq. (4) and (5),

 Δs : Slip

- Y : Increased total length
- E : Modulus of elasticity of threaded steel rod
- ΔL : Increased length of threaded steel rod

P : Load

As : Cross-sectional area of threaded steel rod

Lo : Initial threaded steel rod length

RESULTS AND DISCUSSION

The moisture content on laminated bamboo right after the test was 15.56% based on ASTM (2003). The Specific Gravity test from laminated bamboo referred to the ASTM (2014) with the result of 0.687 g/cm³ that was similar to the research of Malanit *et al.* (2011) with the result of 0.720 g/cm³. The pull-out resistance test results from threaded steel rod with the varying edge distances of 1d, 1.5d, 2d, 2.5d, 3d, 3.5d, 4d, 4.5d obtained the pull-out resistance, the damage types that occurred and slip modulus as explained below.

Threaded steel rod pull-out resistance: In this research, the pull-out resistance results indicated that the minimum distance of threaded steel rod before

decreasing the pull-out strength occurred at 3d edge distance with the value of 19.72 kN and the shear strength, calculated using Eq. (1), was 11.209 MPa. The similar shear strength value was obtained by Yan *et al.* (2016), with the result of about 10.54 MPa. Table 1 lists the complete results of the pull-out resistance test for all varying edge distance.

At the 2.5d edge distance, pull-out resistance and shear strength declined to 17.40 kN and 9.890 MPa. The value drops for 11.76% from 3d edge distance. At a 2d edge distance or less, the pull-out resistance kept declining as observed from Fig. 3.

The drop in pull-out resistance is caused by the splitting failure that occurred in the specimens before the maximum load in the glued-in rod was achieved. Therefore, the load value is lower compared to the specimen with no splitting failure. Figure 3 shows the correlations between edge distance and pull-out resistance results from the test. Whereas Fig. 4 shows the comparison in pull-out resistance between glued-in rod in laminated bamboo with equation approach of the glued-in rod in wood.

Figure 4 indicates that this research results in pullout resistance were similar to the pull-out resistance calculated using the equation of Deng (1997) and

Specimen code	Diameter of treaded rod (mm)	Edge distance (d)	Number of specimen	Types of failure	
				 Pulled	Splitting
S1-d	10	1	5	-	5
S1.5-d	10	1.5	5	1	4
S2-d	10	2	5	5	-
S2.5-d	10	2.5	5	5	-
S3-d	10	3	5	5	-
S3.5-d	10	3.5	5	5	-
S4-d	10	4	5	5	-
S4.5-d	10	4.5	5	5	-



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Fig. 4: Comparison on pull-out resistance

higher than the pull-out resistance calculated using the equation of New Zealand Timber Design Guide (NZW 14085 SC, 2007), or Eq. (2). The dissimilarities were the results of material differentiation. This research used laminated bamboo material while Deng (1997) and New Zealand Timber Design Guide (NZW 14085 SC, 2007) used the wood material. Although varied in pull-out resistance, the trendline that occurred shows an almost similar pattern. The similarity shows that increasing edge distances caused an increase in pull-out resistance. Blass and Laskewitz (1999) stated that the minimum steel rod edge distance in wood specimen before pull-out resistance and shear strength declined was at 2.5d; while Steiger et al. (2006) gave 2.3d distance.

Types of failure in glued-in rod connection: Based on Table 2, samples with the edge distance less than twice the diameter of the threaded rod experienced splitting failure in the laminated bamboo (Fig. 5b). Samples with the edge distance more than or equal to twice the diameter of the threaded rod experienced damaged, such as pulled threaded rod along with bamboo surfaces around the epoxy adhesive (Fig. 5a). From the damage type that occurred, in summary, the minimum threaded rod distance from the outer edge of laminated bamboo to prevent the splitting failure in laminated bamboo was at twice the diameter from the outer edge laminated bamboo.

Research on pull-out resistance in the glued-in rod of wood by Gattesco et al. (2010) stated that splitting failure is the most frequent damage among others.





Fig. 5: Types of failure; (a) Pulled failure and (b) Splitting failure

Preventing this problem requires knowledge on the minimum distance between the steel rod to the specimen's edge. Results from Gattesco et al. (2010) showed that the minimum distance required was 2.3 times the diameter of the steel rod to prevent splitting failure on wood. In this research, the minimum distance required was at 2d towards laminated bamboo.

Slip modulus: Pull-out resistance in glued-in rod resulted in a curve between loads (P) and slip (ΔS) as observed in Fig. 6. Two important things from this figure are the slip modulus and the collapse model.

The almost similar slope shows that the edge distance did not influence the slip modulus from the glued-in rod in this research. In Table 3, the average values of slip modulus calculated by Eq. (3) is between 3.732 kN/mm to 7.768 kN/mm. Maria and Ianakiev (2015) found that the slip modulus was 1.18 kN/mm

Table 3. Result 0	i siip mouulus					
	Threaded rod			Maximum pull-	Slip at max. pull-	
Edge distance	diameter (d)	Anchored length	Initial length	out load	out load (ΔS)	Slip modulus
(e) (mm)	(mm)	(mm)	(Lo) (mm)	(P) kN	(mm)	(K _s) kN/mm
10	10	40	153.0	13.020	2.251	5.681
15	10	40	149.6	14.720	2.325	5.308
20	10	40	150.4	16.320	2.585	7.768
25	10	40	151.8	17.400	2.780	7.197
30	10	40	151.4	19.720	3.321	5.229
35	10	40	151.2	19.400	3.034	5.313
40	10	40	150.6	18.700	2.920	3.732
45	10	40	150.0	19 325	2 879	4 029

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Table 3: Result of slip modulus

Fig. 6: Relationship between load and slip

for a glued-in rod in 60 mm anchored length in Douglas Fir Wood. Verdet *et al.* (2016) tested glued-in rod with epoxy adhesive (Sikadur 330, Sika, Le Bourger, Switzerland) and timber glulam produced from Black Spruce at 20°C temperature resulted in slip modulus of 108 kN/mm. Rossignon and Espion (2008) tested glued-in rod in glulam 160 mm anchored length in Norway Spruce with epoxy adhesive and obtained the initial modulus of 94.6 kN/mm. The main parameter that caused the varieties in the slip modulus from this research and the other mentioned research above was the embedment length, the material and the adhesive that was used.

In this research, the sudden drop of glued-in rod ability to resist the loads identified the brittle failure, as seen in Fig. 6. This type of collapse occurred due to interfacial damage between glue and bamboo that eliminate interfacial shear strength. Gonzalez *et al.* (2016) discovered that glued-in rod with embedment length 7.5 times the diameter of rod experienced a brittle failure, while rod with 10 times diameter embedment experienced a ductile failure. Maria and Ianakiev (2015) found that brittle failure occurred in pull-out resistance of 8 mm diameter glued-in rod in an Oak Timber and Douglas Fir Timber with embedment length 60 mm.

CONCLUSION

Conclusions from this research were as below:

• A minimum distance of threaded steel rod from the outer edge laminated bamboo before experiencing

a decline of pull-out resistance was at 3d, with d was diameter threaded steel rod.

- The splitting failure on laminated bamboo occurred when the edge distance of threaded steel rod was less than 2d, whereas the distance of the threaded steel rod was more than or equal to 2d, the pulled failure of threaded steel rod from laminated bamboo occurred.
- The edge distance did not influence the magnitude of the slip modulus on the threaded steel rod glued-in laminated bamboo.
- The brittle failure occurred in a threaded steel rod glued-in laminated bamboo that experienced splitting or pulled failure.

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CONFLICT OF INTEREST

There's no conflict of interest.

REFERENCES

ASTM (American Society for Testing and Materials), 2003. Standard Test Methods for Direct Moisture Content Measurement of Wood and Wood-Base Materials. Annual Book of ASTM Standards, Vol. 04:10: D 4442-92 Section 2, West Conshohocken, PA, United States.

- ASTM (American Society for Testing and Material), 2014. Standard Test Methods for Density and Specific Gravity (Relative Density) of Wood and Wood-Based Materials. Annual Book of ASTM Standards, Vol. 04:10: D 2395-14 Section 6, West Conshohocken, PA, United States.
- Blass, H.J. and B. Laskewitz, 1999. Effect of spacing and edge distance on the axial strength of glued-in rods. Proceeding of the CIB-W18 Meeting Thirty-Two, Graz, Austria, Aug. 23-25, Paper 32-7-12.
- BS EN 26891, 1991. Timber Structures-Joints Made with Mechanical Fasteners-General Principles for the Determination of Strength and Deformation Characteristics. European Committee for Standardisation (CEN), Brussels, Belgium.
- Deng, J.X., 1997. Strength of epoxy bonded steel connections in glue laminated timber. Ph.D. Thesis, Department of Civil Engineering, University of Canterbury, Christchurch, New Zealand.
- Gattesco, N., A. Gubana and M. Buttazzi, 2010. Pullout strength of bar glued-in-timber joints. Proceeding of 11th Word Conference on Timber Engineering (WCTE). Trentino, Italy, Jun. 20-24, pp: 1194-1200.
- Gonzalez, E., C. Avez and T. Tannert, 2016. Timber joints with multiple glued-in steel rods. J. Adhesion, 92(7-9): 635-651.
- Harte, A., R. Jockwer, M. Stepinac, T. Descamps, V. Rajcic and P. Dietsch, 2015. Reinforcement of timber structures – the route to standardization. Proceeding of 3rd International Conference on Structural Health Assessment of Timber Structures. Wroclaw - Poland, Sep. 9-11, pp: 78-88.
- Karyadi and P.B. Susanto, 2017. Mechanical characteristics of box-section beam made of slicedlaminated Asian bamboo (Dendrocalamus asper) in bending failure mode under transversal load. Proceeding of AIP Conference, American Institute of Physics, Vol. 1887, ID: 020062.
- Karyadi, S.M. Dewi and A. Soehardjono, 2018. The strength of axially loaded square hollow-section column made of laminated Asian bamboo (*Dendrocalamus asper* becker). Res. J. Appl. Sci. Eng. Technol., 15(9): 337-343.
- Malanit, P., M.C. Barbu and A. Frühwald, 2011. Physical and mechanical properties of oriented strand lumber made from an Asian bamboo (*Dendrocalamus asper* backer). Eur. J. Wood Wood Prod., 69(1): 27-36.

- Maria, V.D. and A. Ianakiev, 2015. Adhesive connections in timber: A comparison between rough and smooth wood bonding surfaces. Int. J. Chem. Mol. Nucl. Mater. Metallurgical Eng., 9(3): 395-401.
- NZW 14085 SC, 2007. New Zealand Timber Design Guide. Timber Industry, Federation Inc., Wellington, New Zealand.
- O'Neill, C., D. McPolin, S.E. Taylor, A.M. Harte, C. O'Ceallaigh and K.S. Sikora, 2017. Timber moment connections using glued-in basalt FRP rods. Constr. Build. Mater., 145: 226-235.
- Rossignon, A. and B. Espion, 2008. Experimental assessment of the pull-out strength of single rods bonded in glulam parallel to the grain. Holz Roh Werkst., 66: 419-432.
- Sinha, A., D. Way and S. Mlasko, 2014. Structural performance of glue laminated bamboo beams. J. Struct. Eng., 140(1): 04013021.1-04013021.8.
- Steiger, R., E. Gehri and R. Widmann, 2006. Pull-out strength of axially loaded steel rods bonded in glulam parallel to the grain. Mater. Struct., 40: 69-78.
- Steiger, R., E. Serrano, M. Stepinac, V. Rajčić, C. O'Neill, D. McPolin and R. Widmann, 2015. Strengthening of timber structures with glued-in rods. Constr. Build. Mater., 97: 90-105.
- Stepinac, M., F. Hunger, R. Tomasi, E. Serrano, V. Rajcic and J.W. van de Kuilen, 2013. Comparison of design rules for glued-in rods and design rule proposal for implementation in European standards. Proceeding of CIB - W18 Meeting 46, Vancouver (Canada), Aug. 26-29, pp: 1-13.
- Verdet, M., A. Salenikovich, A. Cointe, J.L. Coureau, P. Galimard, W.M. Toro, P. Blanchet and C. Delisee, 2016. Mechanical performance of polyurethane and epoxy adhesives in connections with glued-in rods at elevated temperatures. BioResources, 11(4): 8200-8214.
- Xiao, Y., Q. Zhou and B. Shan, 2010. Design and construction of modern bamboo bridge. J. Bridge Eng., 15(5): 533-541.
- Yan, Y., H. Liu, X. Zhang and Y. Huang, 2016. The effect of depth and diameter of glued-in rods on pull-out connection strength of bamboo glulam. J. Wood Sci., 62: 109-115.
- Yeboah, D., S. Taylor, D. McPolin and R. Gilfillan, 2013. Pull-out behaviour of axially loaded Basalt Fibre Reinforced Polymer (BFRP) rods bonded perpendicular to the grain of glulam elements. Constr. Build. Mater., 38(5): 962-969.