

## Research Article

### **Confluence Dynamics in an Ephemeral Gully Basin (A Case Study at Rangamati, Paschim Medinipur, West Bengal, India)**

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**Abstract:** Despite many efforts over the last decades to understand confluence angles of rill or gully, they remain unclear. This paper presents the results of gully confluence angles developed at Rangamati ephemeral gully basin of Paschim Medinipur District, West Bengal in India. The confluence angles are monitored for 3 years (2007-2009) and gradient, discharge and stream power of both parent and tributary stream are measured at each junction. Calibrating the data to existing models shows that Optimal Confluence model (Roy, 1983) is better applicable to the present study where average value of symmetry ratio becomes, 0.300 and the value of exponent 'x' becomes -0.20. The plot experiment at laboratory under simulated rain shows the tendency of Tran's link development and downward migration of the lower most junctions due to availability of maximum discharge under constant slope condition. In the situation of homogeneous soil resistance, equal distributed rain and general gradient, local variation of energy is observed due to localized erosion or deposition and associated local variation of gradient in micro scale. Angles of junction are changed in response to the variation of gradient (S), discharge (Q) and Sediment Yield (SY). These changes are episodic in nature and so no average rate can be estimated. The junction migrates both upstream and downstream depending on the relative importance of deposition, erosion and associated change in junction angle.

**Keywords:** Confluence angle, confluence migration, discharge, gradient, symmetry ratio, sediment yield

## INTRODUCTION

Confluences are very complex fluvial networks where the combination of matter (water and sediment) and energy (flow strength) from two different channels take place (Roy, 2008). Stream junction angles are important morphometric and geometric property of channel networks as it regulates the flow from a tributary to the receiving stream. The angles of junction are controlled by erosion and sedimentation at the confluence with time (Schumm, 1956) and by the gradient of the receiving and the tributary stream (Horton, 1945). The influence of the gradient of the two merging streams is reflected by relative importance of either erosion or deposition at or near the junction. The angle of junction varies inversely with the relief. Moreover, the angle of junction increases as the order of the receiving stream increases (Lubowe, 1964). It is related to discharge of the two tributary streams (Howard, 1971c) and discharge per unit width (Mosley, 1976). The discharge, gully width, gully depth, runoff contributing area and gradient are the important factors of gully network system. The river confluences are

critical nodes in river systems where tributary fluxes of water and sediment can elicit adjustments in the geomorphology, hydraulics, sedimentology and ecology of the recipient channel (Abrahams, 1984; Rhoads, 1987; Paola *et al.*, 2006; Biron and Lane, 2008).

The present work monitors the drainage network dynamics through field study and Laboratory experiment by assessing the gradient, discharge, width and depth along both tributary and mainstream both upstream and downstream of the junctions. The confluence angles are also linked with the influence of varied condition of the catchment area. The major aim of the present research is to have cognition of the inter-working of processes leading to the development and variation of junction angles and the migration of confluences. In this process, the collected data are calibrated to the recognized models to make a comparative suitability test for understanding the association of factors working at confluences. Plot experiment with simulation rainfall is made to assess the mechanism of network development through the change in links and nodes (junctions).

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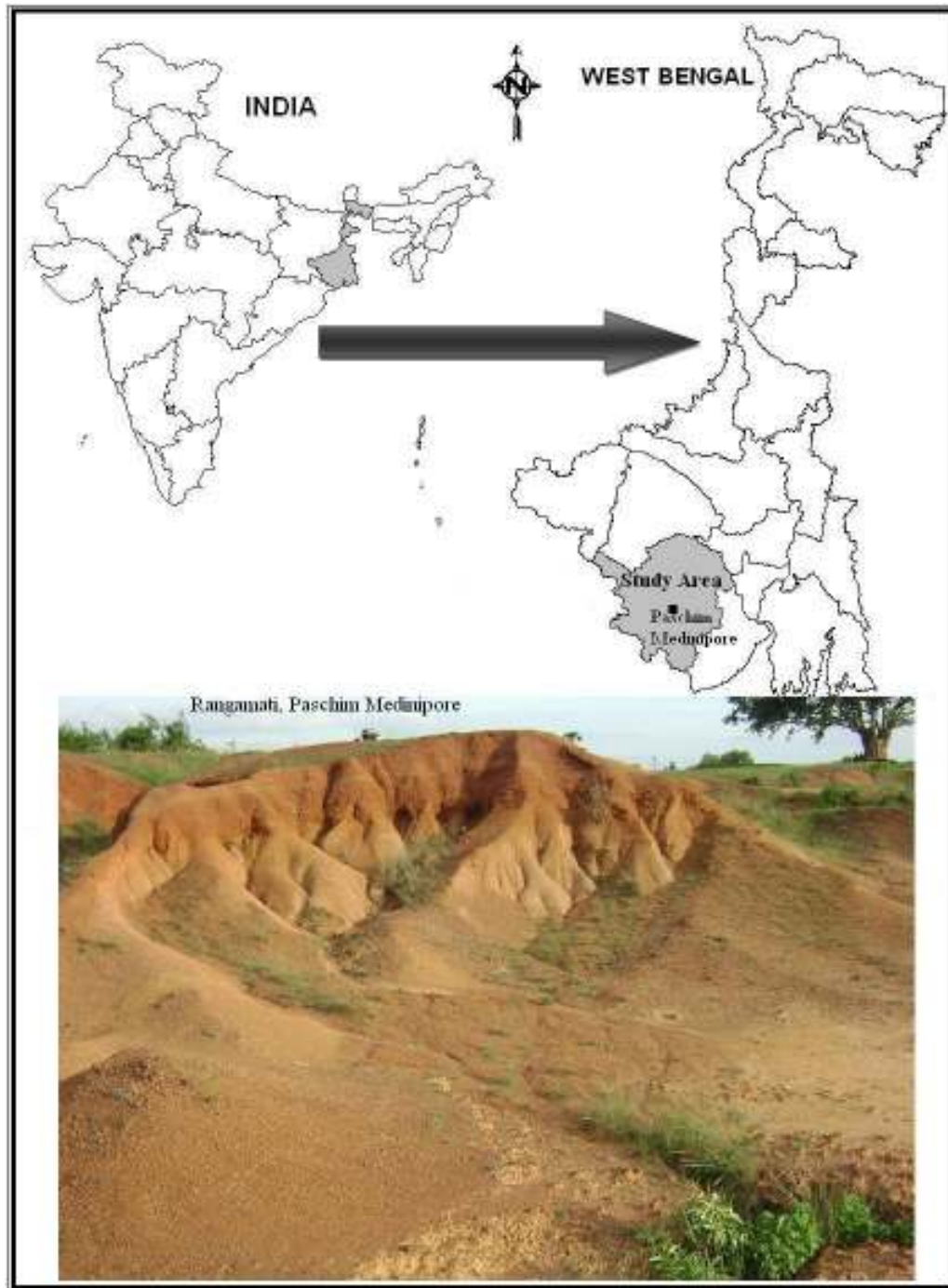


Fig. 1: The study area of 256 sq m encompasses an ephemeral discontinuous basin developed on lateritic soil; the upper catchment with steep slope shows more erosion and associated headward extension of gully heads with toppling failure; the channels are partially filled at lower catchment by sediments brought from upslope; channel network is frequently changed by adjustment with the continuously changing distribution and redistribution of mass (sediments) with variation in availability of energy (power) within the basin

#### **GEOGRAPHIC AND GEOMORPHIC SETTINGS**

The current research has been carried out in the lateritic western part of West Bengal, India, on the bank of river

Kossi. A representative Ranganati Gully catchment of 256 sq m ( $22^{\circ} 24' 42.0''$  N to  $22^{\circ} 24' 43.2''$  N and  $87^{\circ} 17' 48.1''$  E to  $87^{\circ} 17' 48.09''$  E) from this region was selected for present study (Fig. 1). A tropical, monsoonal climate prevails in with mean annual

temperature of around 28.4°C and the average summer (May) and winter (December) temperatures of 40.9° and 7.5°C respectively. The mean annual rainfall is about 1850 mm. Rainfall distribution is irregular, experiencing high-intensity rainstorms during June to September (i.e., >125 mm/h over short periods), with high erosive potential (the rainfall erosive factor *R* varies between 1200 and 1500 MJ mm/ha/h year). The major part of soil profiles has been truncated by hydraulic erosion and underlying horizons constitute, at present, the top layers (Shit and Maiti, 2008). One of the main characteristics of the area is the dissection of the landscape by a dense and deep network of rill and gullies. Inter-gully areas are usually undulating and rolling. The average slope of this area is between 25 and 35%. The most frequent landforms are complex slopes and gullies. The rills are characterized by vertical sidewalls of 7 -13cm and are 90 cm wide. Rill has a high degree of lateral as well as head retreat. The nick points, developed at the vertical head near the source, sometimes show the tension cracks for toppling, where centre of gravity overlies the centre of mass (Shit and Maiti, 2008). Sediment mobilized from the walls and vertical heads is usually removed by flowing water during high intensity rainstorms. In other cases, the sediments are deposited on the walls or on the gully bottom, which may lead to some degree of stabilization. Major part of the destabilized sediment is deposited at the lower catchment that makes the gully discontinuous. Major shift of the channels and junctions are observed on these deposits in response to the variation of discharge and load.

**BACKGROUND AND MATHEMATICAL DEVELOPMENT**

The regularity of the angular relations at stream junctions was recognized early in the development of geomorphology by Playfair (1802) who noted that “..... this law is in general observed, that where a higher (steeper) valley joins a lower (gentler) one, of the two angled which it makes with the latter, that which is obtuse is always on the descending side; a law that is the same with that which regulates the confluence of streams running on a surface nearly of uniform inclination” (Howard, 1971). Horton (1932, 1945) proposed, for the first time, that the junction angle ( $\emptyset$ ) depends solely on the ratio of main stream gradient to that of the tributary Eq. (1).

$$\text{Cos}\emptyset = S_m / S_t \tag{1}$$

where,  $S_m$  and  $S_t$  are the gradients of the main and tributary streams, respectively.

Lubowe (1964), after testing Horton’s model concluded that it is predictive of the junction angles

close to actual ‘except for the junction of streams of the same order’ with same gradient.

Howard (1971c) modified Horton’s model and divided the junction angle (*T*) into two by extending the receiving link up slope and are named as  $E_1$  &  $E_2$  in correspondence to the joining link 1 and 2, respectively. The receiving stream is marked as link 3. The angle  $E_1$  and  $E_2$  are calculated following Horton’s rule:

$$T = E_1 + E_2 \tag{2}$$

where,

$$\text{Cos}E_1 = S_3 / S_1 \tag{3}$$

$$\text{Cos}E_2 = S_3 / S_2 \tag{4}$$

The entrance angle  $E_1$  and  $E_2$ , measured in the horizontal plane, lie between the prolongation of the receiving stream at each junction and the smaller and larger tributaries, respectively and  $S_1$ ,  $S_2$  and  $S_3$  are the gradients of the smaller and larger tributaries and the receiving stream, respectively.

Howard (1971) suggested for minimum power function in connection to the flow geometry in transport network. These links will join at a point where the total power cost ( $\Omega$ ) is minimum and is calculated by the sum of the costs per unit length ( $C_i$ ) over three links multiplied by the segment length ( $L_i$ ):

$$\Omega = \sum_{i=1}^3 C_i L_i \tag{5}$$

$$C_i L_i = \rho g Q_i S_i \tag{6}$$

where,

$\rho$  = Fluid density

$g$  = Gravitational acceleration

$Q_i$  = discharge flowing through the channel segment

$S_i$  = Channel gradient

Mosley (1976) proposed that the junction angle responds to the velocities of incoming links to conserve lateral momentum of the incoming flows:

$$Q_1 V_1 \sin E_1 = Q_2 V_2 \sin E_2 \tag{7}$$

where,  $Q_1$  and  $Q_2$  are the discharge of tributary 1 and 2;  $E_1$  and  $E_2$  are the angles (Howard, 1971c).

Roy (1983) and Woldenberg and Horsfield (1983, 1986) linked minimum power with the junction angles being independent of the lengths ( $L_i$ ).

$$\text{Cos}E_1 = \frac{(C_3^2 + C_1^2 - C_2^2)}{2C_1 C_3} \tag{8}$$

$$\text{Cos}E_2 = \frac{(C_3^2 + C_2^2 - C_1^2)}{2C_2 C_3} \tag{9}$$

where,  $C_1$ ,  $C_2$  and  $C_3$  are the weights per unit length assigned to the smaller and larger tributaries and the receiving stream, respectively.

The discharge from the tributaries is considered to be collected along the receiving link through continuity equation:

$$Q_3 = Q_1 + Q_2 \quad (10)$$

A symmetry ratio is thus proposed for determining the variable hydro-geomorphic conditions along the tributary links.

$$\alpha = Q_1 / Q_2 \text{ (where, } Q_1 \leq Q_2 \text{)} \quad (11)$$

and Eq. (8), (9), (10) and (11) are combined to obtain:

$$\cos E_1 = \frac{(1 + \alpha)^{2X} + \alpha^{2X} - 1}{2\alpha^X (1 + \alpha)^X} \quad (12)$$

$$\cos E_2 = \frac{(1 + \alpha)^{2X} + 1 - \alpha^{2X}}{2(1 + \alpha)^X} \quad (13)$$

where,  
 $X$  = The exponent

Following Eq. (2), the combination of  $E_1$  and  $E_2$  gives rise to the junction angle ( $T$ ).

### MATERIALS AND METHODS

The initial drainage network as on March, 2007 was mapped in details, by Total Station, tape, compass and level. The links and their junctions were numbered and given the permanent identity for keeping the records and monitoring the changes over time. The additional and decayed links and junctions were also recorded. The repetitive field surveys since 2007 were made to monitor the changes and to assess the mechanism involved in such changes. Major changes were recorded during the surveys on 2<sup>nd</sup> September, 2007, 26<sup>th</sup> June, 2009 and 12<sup>th</sup> September, 2009. The junction angles were measured in the field following Jarvis (1976) and Flarity (1978) to monitor the angular components of the drainage network. The angle of junction was studied following Schumm (1956) to understand the nature of association among the factors operating at or near the junctions, responsible for spatio-temporal change in junction angle and its position. The gradient of each link above each junction was monitored prior and after the high intensity rains and were recorded to monitor any change in response to relative erosion and deposition within the channels. The



Fig. 2: (a) Monitoring junction angle and gradient of the merging links in field, (b) measurement of infiltration in field through a plot of 1×1 feet area with regulated supply of water for duration of 5 h. until a constant rate is reached following (Goudie, 1990), (c) collection of water and sediment discharge at the gully mouth during a rain, recorded by rain gauge. The infiltrated water was also collected simultaneously from the base of a representative plot (1 m × 1 m) set the field with an average gradient for comparison with the former. Only little variation is observed between these two methods, (d) Monitoring discharge by setting ‘V’ notch at each junction connected with the bottles for collection of entire flow of water and sediment; the rain input is recorded in the field with recording type rain gauge

gradient (S) and discharge (Q) of the incoming links above each junction are measured in the field respectively by clinometers and 'V' notch set with impermeable clay (Fig. 2). The discharge from the prominent rains (quantified at the field by rain gauge, Fig. 2) was collected at each confluence and it's recorded. The rate of infiltration was measured in the field following Goudie (1990) (Fig. 2B). The collected discharge was analyzed to quantify the water and sediment component, in relation to rain intensity, contributing area, gradient and stream power (Torri *et al.*, 2006). The shifting of the confluences was monitored by pegging techniques and associated change in junction angles were recorded and linked with relative importance of erosion and deposition at confluences. The mechanism of change in junction angle and shift of the confluence was studied through plot experiment under simulated rain condition (Gomez and Mullen, 1992; Berger *et al.*, 2010) (Fig. 7). The plot of 1m x 1m is prepared with the soil collected from concerned study area and is exposed in open air for nearly six months for sufficient compaction in an attempt to prepare a situation similar to that of field area. The rain is dropped from 5 m distance over head at the constant intensity that is observed during last five years on an average. The plot was set at 20° initial gradient, the average of the field area. The experiment was continued for seven hours. The changes in the network as well as junctions were recorded at 1 h interval and mapped accordingly. The prediction of angles of junction are made following Horton (1932, 1945), Lubowe (1964), Howard (1971, 1971c) and Roy (1983). The observed data were used for calculating expected confluence angles after Horton (1945), Howard (1971, 1971c) and Roy (1983). The comparative validity testing of the models were made by comparing the expected angels to that of observed using SPSS software.

## THE RESULTS AND DISCUSSION

**Network dynamics:** The gully basin under study showed remarkable change in the network that were revealed during field survey. These changes were episodic in nature and occurred in response to threshold conditions and were observed after catastrophic rains. The spatial variation in the network dynamics was linked with watershed zones. Maximum rate of lengthening of the links by headward extension were observed in sediment source zone (Laity and Malin, 1985). Minor channels were developed by concentration of overland flow that developed fresh bifurcation and branching during monitoring period. The sediment and water transfer zone depicted the change in confluence angle as well as width and depth of the channels. The depth was increased at the



Fig. 3: The gully basin under survey, as on 09.03.2007 showed the orientation of links and distribution of junctions

upper catchment but decreased at the lower section due to partial filling. The channel network showed constant adjustment to the changing conditions brought by the high intensity rains (Bruno *et al.*, 2008). The angular component of the network, the confluence angle, was changed in response to the intensity of erosion and deposition near the confluence and surrounding region. Except for few junctions most of the angles registered a positive growth during the rains in 2007 and these were decreased by June, 2009 and subsequently increased in the rainy days of 2009. Additional links the mainly shoe-string gullies were developed from gully wall and some of the minor links were obliterated by cross grading also (Shit and Maiti, 2009). The link OP was obliterated due to cross grading of GB along its right bank during June- September, 2009 (Fig. 6A, B).

The sediment sink zone, the lower reach, being characterized with low gradient, showed huge sedimentation and resultant closure of earlier channels and subsequent re-excavation during intensified rain. The prominent braiding was observed during post monsoon (September) of 2007 and after wards more sediment was deposited to cover the entire architecture. Two prominent channels were re-established leaving the debris at the centre thus the deposits are getting larger and higher by both lateral and upward growth (Fig. 3).

**Confluence hydrology:** All the confluences were monitored for a quite long duration. The result of recent survey on 12<sup>th</sup> September, 2009 is presented in Table 1. Discharge at the junction point largely depends on the contributing area of the merging streams, gradient and permeability of the catchment. The hour wise rain fall data was not available and so the arrangement was made to record the rain intensity at field by recording type rain gauge (Fig. 2C, D) Simultaneous measurement of infiltration and runoff (Fig. 2B, C) were taken to correlate with rain input. The records of the results at each junction point was arranged

Table 1: Hydro geomorphic characters of the confluences during a catastrophic rain (17.64 mm/h) on 12<sup>th</sup> September, 2009 with initial infiltration rate of 11 mm/h, and terminal rate of 1.2 mm/h; confluence 'I' and 'K' received huge water discharge as a result of larger contributing area; inspite of smaller catchment area, sediment yield is high at 'C' junction

Junctions name	Receiving stream		Tributary stream		Gradient (along the joined flow)	Contributing area m <sup>2</sup> (during natural flow)	Channel width (cm)	Channel depth (cm)	Junction angle in degree	Water discharge (cm <sup>3</sup> /sec)	Sediment Yield (kg m <sup>-2</sup> )
	Links	Gradient	Links	Gradient							
C <sub>20</sub>	C <sub>20</sub> J	11	C <sub>20</sub> N <sub>20</sub>	25	8	11.813	22	4.5	72	9.793	0.029543723
C <sub>21</sub>	C <sub>21</sub> J	8	C <sub>21</sub> N <sub>21</sub>	28	16	5.310	30	5.6	62	2.916	0.064971751
C <sub>25</sub>	C <sub>25</sub> J	20	C <sub>25</sub> N <sub>25</sub>	48	22	4.350	14	2.2	62	2.302	0.056469433
C <sub>1</sub>	C <sub>1</sub> J	18	C <sub>1</sub> N <sub>1</sub>	35	20	4.073	17	4.2	58	1.854	0.049908925
C <sub>2</sub>	C <sub>2</sub> J	24	C <sub>2</sub> N <sub>2</sub>	44	23	2.745	16	2.8	62	1.614	0.415308642
C <sub>26</sub>	C <sub>26</sub> J	24	C <sub>26</sub> N <sub>26</sub>	42	28	2.104	17	2.2	56	1.375	0.072222222
C <sub>3</sub>	C <sub>3</sub> J	20	C <sub>3</sub> N <sub>3</sub>	47	24	2.025	12	4.0	70	0.949	0.000517129
C <sub>4</sub>	C <sub>4</sub> J	29	C <sub>4</sub> N <sub>4</sub>	35	24	1.800	18	4.6	69	0.625	0.009284776
I	IB	7	IJ	9	6	243.653	22	4.5	65	63.122	0.006791778
G	GB	10	GH	14	6	54.067	28	13.4	53	44.219	0.021668397
C <sub>23</sub>	C <sub>23</sub> H	14	C <sub>23</sub> N <sub>23</sub>	16	8	16.785	32	3.4	65	14.584	0.111689351
C <sub>6</sub>	C <sub>6</sub> H	12	C <sub>6</sub> N <sub>6</sub>	18	13	14.445	26	9.6	72	10.937	0.162145242
C <sub>7</sub>	C <sub>7</sub> N <sub>6</sub>	29	C <sub>6</sub> N <sub>6</sub>	30	25	2.498	20	6.0	56	3.333	0.014347079
C <sub>5</sub>	C <sub>5</sub> H	35	C <sub>5</sub> N <sub>5</sub>	40	34	4.792	14	3.0	36	3.021	0.001360456
C <sub>8</sub>	C <sub>8</sub> B	10	C <sub>8</sub> N <sub>8</sub>	15	15	34.920	17	4.0	62	21.875	0.006500389
E	EB	40	EF	53	30	28.306	9	7.4	25	2.917	0.327868852
C <sub>24</sub>	C <sub>24</sub> F	22	C <sub>24</sub> N <sub>24</sub>	30	25	4.478	33	3.2	-	5.253	0.063161663
C <sub>9</sub>	C <sub>9</sub> F	-	C <sub>9</sub> N <sub>9</sub>	-	-	2.745	-	-	75	1.979	0.028070175
E <sub>1</sub>	E <sub>1</sub> B	10	E <sub>1</sub> F <sub>1</sub>	35	8	19.553	25	3.8	55	11.458	0.101017861
C	CB	10	CD	14	20	12.825	35	2.0	75	9.031	1.108651087
C <sub>1</sub>	C <sub>1</sub> B	25	C <sub>1</sub> D <sub>1</sub>	32	22	5.207	21	4.7	45	5.313	0.001245724
C <sub>10</sub>	C <sub>10</sub> B	20	C <sub>10</sub> N <sub>10</sub>	42	22	2.439	14	1.2	65	3.385	0.007870507
K <sub>1</sub>	K <sub>1</sub> B	-	K <sub>1</sub> L	-	-	246.443	-	-	-	16.412	0.017638656
K	KB	6	KL	8	2	152.595	14	3.9	56	115.938	0.040502931
C <sub>22</sub>	C <sub>22</sub> L	6	C <sub>22</sub> N <sub>22</sub>	9	4.5	80.505	30	4.0	50	27.605	0.037690747
V	VL	14	VU	18	10	35.977	15	4.0	60	10.833	0.314336918
C <sub>13</sub>	C <sub>13</sub> U	12	C <sub>13</sub> N <sub>13</sub>	17	14	8.370	11	1.8	36	0.73	0.155824508
C <sub>19</sub>	C <sub>19</sub> U	22	C <sub>19</sub> N <sub>19</sub>	23	12	5.288	105	2.9	70	0.391	0.065418227
C <sub>11</sub>	C <sub>11</sub> U	22	C <sub>11</sub> N <sub>11</sub>	26	12	4.005	105	3.0	65	0.260	0.191423002
C <sub>12</sub>	C <sub>12</sub> U	36	C <sub>12</sub> N <sub>12</sub>	45	21	2.565	12	1.8	52	0.167	0.010107015
M	ML	14	MN	17	7	70.785	16	3.4	62	25.00	0.614965986
T	TL	10	TS	19	10	13.456	11	2.8	60	10.105	0.147311828
C <sub>14</sub>	C <sub>14</sub> S	20	C <sub>14</sub> N <sub>14</sub>	35	22	2.205	18	3.0	72	1.395	0.642374789
C <sub>15</sub>	C <sub>15</sub> L	11	C <sub>15</sub> N <sub>15</sub>	26	22	5.580	16	3.0	50	4.583	0.034023464
X <sub>1</sub>	X <sub>1</sub> L	-	X <sub>1</sub> Y <sub>1</sub>	-	-	3.554	-	-	-	2.670	0.045766289
C <sub>16</sub>	C <sub>16</sub> N	11	C <sub>16</sub> N <sub>16</sub>	22	8	14.490	20	3.0	-	5.209	0.123279817
O <sub>2</sub>	O <sub>2</sub> N	22	O <sub>2</sub> O <sub>1</sub>	26	18	7.582	14	4.0	50	3.646	0.184182015
C <sub>18</sub>	C <sub>18</sub> N	32	C <sub>18</sub> N <sub>18</sub>	42	42	3.488	9	6.0	55	1.667	0.185185185
C <sub>17</sub>	C <sub>17</sub> O <sub>1</sub>	-	C <sub>17</sub> N <sub>17</sub>	-	-	1.846	-	-	48	1.651	0.178837556

and linked with other hydro-geomorphic elements like contributing area, channel width, channel depth at junction, gradient, water discharge from the particular rain, sediment yield etc following Roy and Sinha (2007) (Table 1).

The tributary following steep gradient supplied more sediment at junction (Vanwalleghem *et al.*, 2005). The monitoring at each junction through tapping the water and sediment yield did not allow measuring the contributions from upslope junctions and thus the contribution of the concerned tributary and limited part of the receiving stream just below the tapped junction was responsible for the results recorded at each junction (Table 2). The gradient and discharge along the tributary thus played important role in sediment yield at each junction. But during natural flow, successive downstream junctions experience discharge from additional larger cumulative contributing area. The deposition or erosion at the junction were controlled by the amount of sediment yield and associated conditions for removal power guided by the discharge and gradient (Best, 1986; Rice *et al.*, 2001, 2006). The possibility of confluence migration depends on the intensity of

sediment yield and cross section area that accommodates this sediment and the power of the stream for removing this sediment (Howard, 1971; Mosley, 1976). In spite of receiving greater discharge, the junction E, I and K showed huge deposition (Table 1) as the sediments could not be removed due to low gradient and so, these experienced considerable migration (Table 1).

Although the junctions like M, O<sub>2</sub>, C<sub>6</sub> and T received considerable sediment discharge, efficient removal due to sufficient gradient developed erosion environment near the junction (Table 2) (Benda, 2008). Junction M, in spite of having low gradient, sufficient discharge helped to remove the sediment coming from large contributing area.

**Confluence migration:** Confluence point showed remarkable migration both up and down slope depending on the relative rate of erosion and deposition as well as orientation of incoming streams (Sanchis *et al.*, 2009) (Fig. 10). Junction 'V' registered an upstream migration after the rainy season of 2009 as some catastrophic rain capacitated 'VT' link to

Table 2: Confluence dynamics: change in confluence angle and associated migration as a response to the change in length, width, depth, gradient and contributing area of the merging links; the junction 'E' showed considerable downstream migration due to huge deposition (up stream of junction) and associated shortening of links, reduction of width, depth, contributing area and confluence angle; a gradual downstream migration is also recorded at 'M' Upstream shifting of 'K' was recorded during 02.09.2007-26.06.2009 due to deposition and associated increase in mean length, width and contributing area of the links; gradient drastically decreased during that period; subsequently revamped energy started erosion with an increase of gradient, as a result, width and depth of the links; confluence angle decreased by three degree and the junction was shifted downstream

Confluences Points	Period (DD/MM/YY)	Max. rainfall intensity	Characteristics of confluence points in fluvial network (ephemeral gully)							Migration (cm)		Causes of confluence migration
			Length Change (cm)	Mean width change (cm)	Mean depth change (cm)	Micro relief change (m)	Contributing area(m2)	Slope (degree)	Confluencesangle (deg)	Up stream	Down stream	
I C16	09/03/07-02/09/07		30.19	29.73	4.94	3.79	95.177	6.5	35			
	02/09/07-26/06/09		43.51	63.0	4.67	3.67	241.259	3.0	69			
	26/06/09-12/09/09		26.05	20.5	4.50	3.32	243.653	10.5	51	x	15	deposition
	09/03/07-02/09/07		-	-	-	-	-	-	-	-	-	-
	02/09/07-26/06/09		6.45	12.5	3.5	1.93	14.917	19	60			
V	26/06/09-12/09/09		5.75	15.5	3.0	1.78	7.582	20.5	50	40	x	Straightening of MN
	09/03/07-02/09/07		20.43	27.12	5.34	3.46	68.330	15.0	30			
	02/09/07-26/06/09		17.40	15.00	4.53	3.43	48.645	12.5	56			
E	26/06/09-12/09/09		13.94	17.50	4.00	3.35	35.977	13.5	30	57	x	Straightening of VL and deposition
	09/03/07-02/09/07		8.79	30.90	9.45	1.20	24.230	13.5	45			
	02/09/07-26/06/09		8.71	37.00	7.64	1.18	25.852	15.5	60			
G	26/06/09-12/09/09		7.30	39.50	7.4	1.08	28.306	14.5	56	x	210	deposition and subsequent erosion
	09/03/07-02/09/07		16.70	25.07	14.86	3.12	55.575	11.0	58			
	02/09/07-26/06/09		16.74	30.50	19.42	3.07	55.117	19.0	47			
C7	26/06/09-12/09/09		14.50	36.50	13.40	2.94	54.067	19.0	49	x	23	erosion
	09/03/07-02/09/07		1.50	17.53	6.81	0.55	2.317	25.5	40			
	02/09/07-26/06/09		3.22	21.5	6.45	0.52	2.385	27.0	30			
M	26/06/09-12/09/09		2.32	10.5	6.00	0.50	2.498	30.5	25	x	10	erosion
	09/03/07-02/09/07		15.88	18.07	4.95	2.85	39.982	12.0	32			
	02/09/07-26/06/09		21.67	24.00	3.91	2.74	40.365	16.5	65	x	125	erosion
O2	26/06/09-12/09/09		18.05	29.00	3.40	2.65	70.785	8.5	55	x	30	erosion
	09/03/07-02/09/07		6.35	26.6	3.43	1.14	10.169	21.5	55			
	02/09/07-26/06/09		5.43	10.00	3.91	1.07	8.077	18.5	55			
C6	26/06/09-12/09/09		9.0	12.5	4.00	0.94	7.582	25.5	60	6.4	x	erosion
	09/03/07-02/09/07		6.46	21.05	7.25	2.95	15.119	20.0	45			
	02/09/07-26/06/09		7.88	18.50	11.21	2.64	11.270	21.5	60	13	x	erosion
K	26/06/09-12/09/09		7.85	18.00	9.60	2.47	14.445	23.5	45	x	10	erosion
	09/03/07-02/09/07		38.48	31.5	4.35	4.12	207.924	9.0	40			
	02/09/07-26/06/09		42.92	95.0	4.12	4.03	238.996	1.5	45	22	x	deposition
T	26/06/09-12/09/09		39.35	49.5	3.90	3.90	246.443	2.5	42	x	60	erosion
	09/03/07-02/09/07		9.30	25.76	3.20	2.65	12.734	17.5	36			
	02/09/07-26/06/09		9.73	18.00	2.98	2.55	12.286	15.5	50	x	12	erosion
	26/06/09-12/09/09		9.00	15.5	2.80	2.21	13.456	15.0	65	x	23	Erosion

straighten its flow. The angle at 'V' registered a growth of 100% from earlier 30°. The junction angle C<sub>16</sub> showed up-slope migration due to straightening of link 'MN' (Fig. 9). The junction 'I' showed a remarkable variation due to huge deposition and subsequent re-excitation (Fig. 6A, B). The deposits covered the entire region during monsoon of 2007 and new shallow channels were developed on the deposits. The link IJ took a further downstream journey avoiding the deposits to join the mainstream at a downstream location. During June, 2009 it was observed that the link GI took a straight course to join IJ at I<sub>1</sub>. After the rain in 2009, in September, all the minor channels were obscured and former orientation, as observed on 09.02.2007, that conveyed the entire contribution of IB segment to JK section, was reestablished. Migration of the junction angles, I, set remarkable variation in confluence hydrology also. Huge deposition and associated avulsion of 'IJ' link during Sept., 07 to June, 2009 led to huge braiding and thus 'I' junction was shifted downstream and received the drainage from a huge additional area and as a response, its confluence angle was increased by almost 100%. The confluence angle 'I' registered a considerable reduction after wards.

The downstream migration of the junction angle was due to the lowering of confluence angles that

creates a flow separation (Best and Reid, 1984) developing a condition of deposition near the confluence region. This raised the geomorphic surface between the two rivers and thus the confluence point moved and downstream migration of the junction was possible (Roy and Sinha, 2007). The junction 'I' revealed downstream migration associated to deposition above the junction, that caused the elevation of the inter-stream area during September, 2007 to June, 2009. The junction 'K' was pushed down ward by a huge deposit during monsoon, 2009 that obscured all the minor links. The earlier channel network was re-established causing a separation of IJ and KL to avoid the huge inter-stream deposition. In the present study, most of the upstream migrations of the junction points were observed in association to active deposition at the sediment sink zone. Huge deposition below the junction pushed the junction angle upstream (K) that indicated the inability of the flow to remove the deposits downstream on low gradient. The junction M registered remarkable migration due to active lateral erosion on the left bank of MN and thus a considerable change (>100%) in the junction angle was recorded. MN link became straight in this process during the monitoring period. Some of the other junctions registered downstream migration also. The junction E showed a remarkable downstream shift (210 cm) during monsoon, 2009. Channel EF shifted right ward by re-

excavating its channel along the margin of the huge deposits that once covered the junction (Fig. 8). In this process, instead of joining AB directly, EF now

contributes via a smaller tributary C<sub>8</sub>N<sub>8</sub>. The junction C<sub>1</sub> and C<sub>7</sub> migrated down slope by active erosion at confluence.

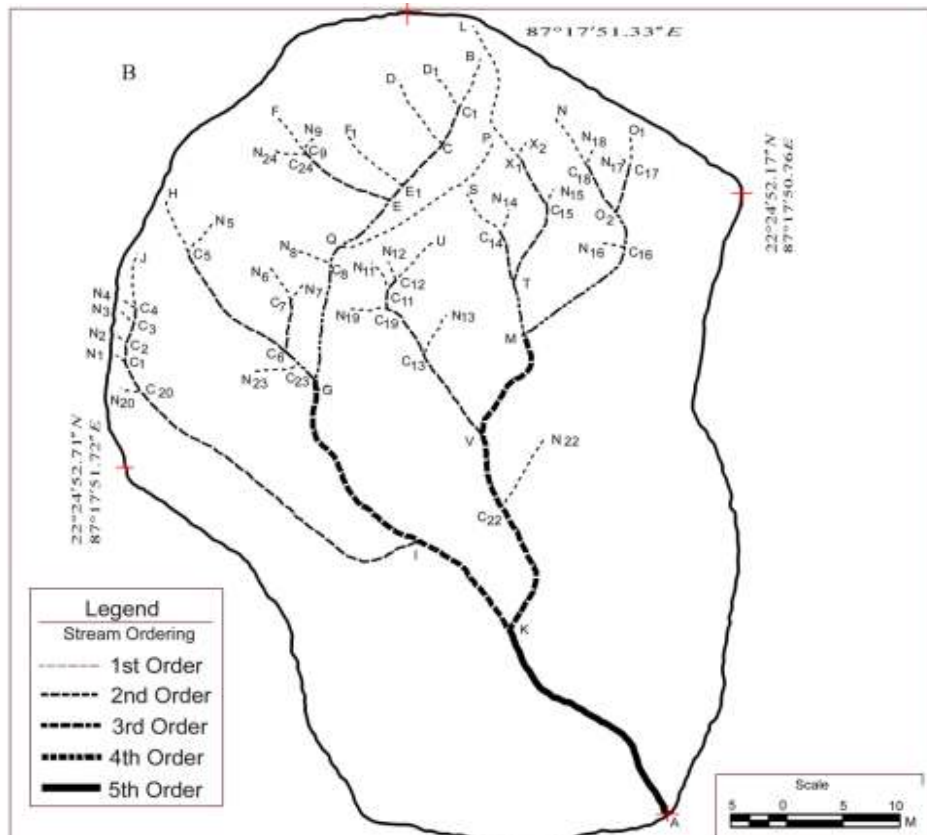


Fig. 4: (a) The gully basin as on 02.09.2007 showed remarkable change both at upper and lower catchments, (b)The additional branches were developed during the monsoon rain of 2007. Some of the links extended headward. The deposit led to braiding and the junctions at the sediment sink zone shifted downward.



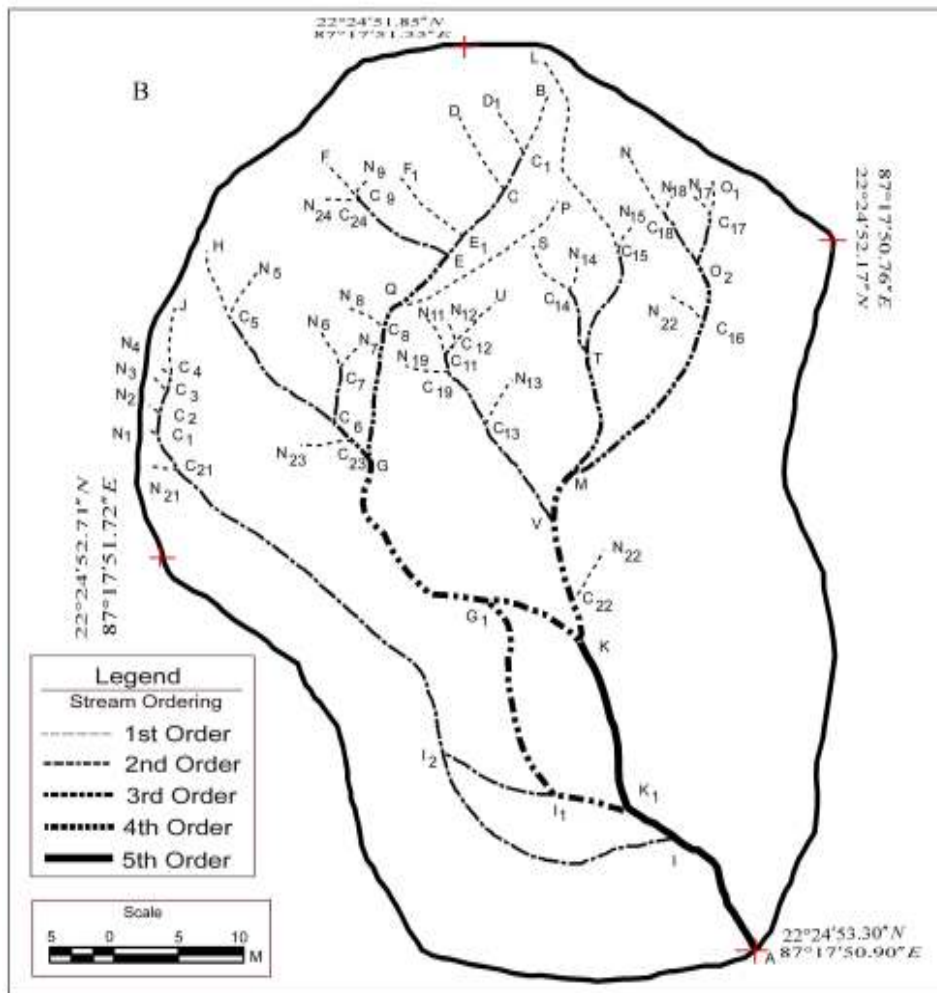


Fig. 5: By 26.06.2009 the basin experienced further braiding due to additional sedimentation at lower catchment

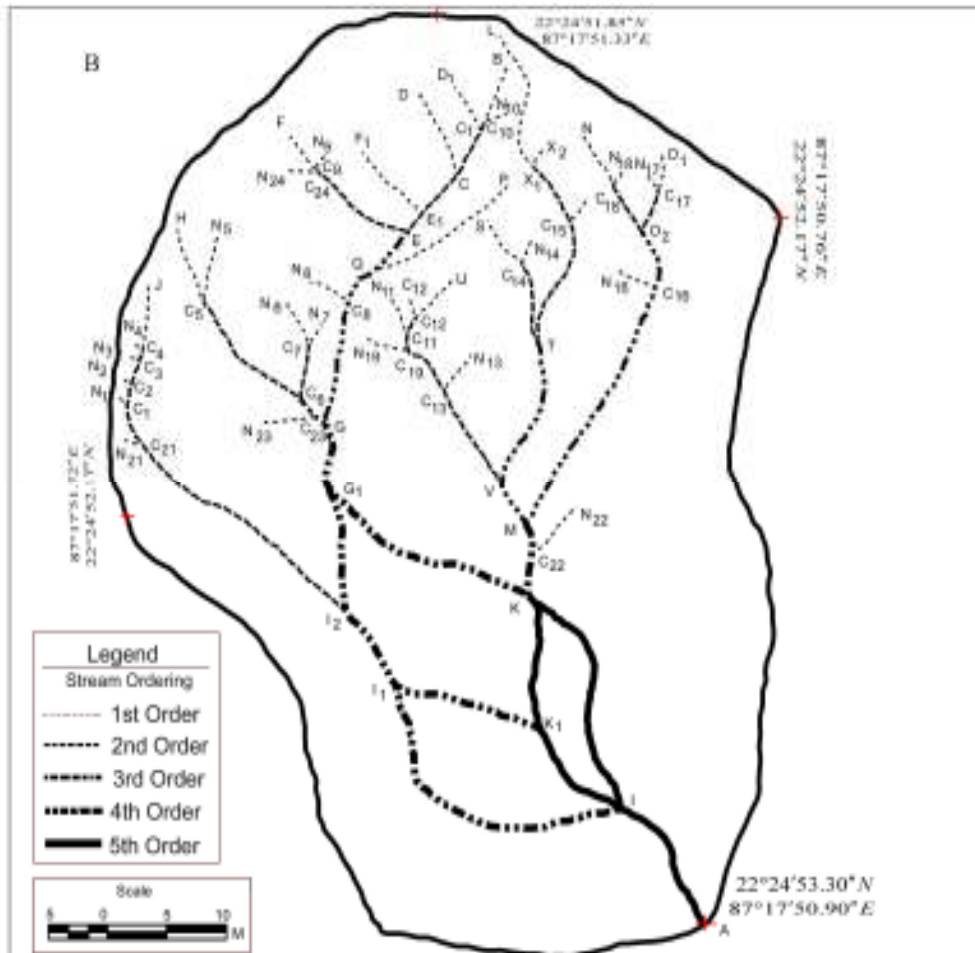


Fig. 6: Re-establishment of the earlier drainage orientation

In the present study the junction angles showed huge variation from time to time (Fig. 6A, B and Table 3). Any change in the relative gradient of tributary and mainstream and that of the discharge by flow intervention along both the streams might cause a change in the confluence angle. This in turn, might regulate the intensity of either deposition or erosion ultimately leading to the change of confluence angle. The variable intensity of rain might be responsible for such variation. Thus the shifting of junctions and associated change in the confluence angles are the results of variety of causes resulting from the association of relief, gradient, runoff contributing area and orientation of links that vary both spatially

according to the location within a basin as well as temporally due to variation in rain intensity (Sanchis *et al.*, 2009) (Fig. 3, 4, 5 and 6).

**Plot experiment to monitor confluence angles:** A plot experiment was done under simulated rain 16.5 mm/h on 1 m×1 m plot set at 20° gradient (Fig. 7 and Table 4). The soil from the concerned study area was collected and compacted for sufficient time to get the resistance comparable to that of the study area. During initial period, the sheet wash with laminar flow was dominant. The drainage links started developing by the concentration of runoff from upslope area at lower reach. Steady increases in the length of the links were

Table 3: Comparison of the accepted models for effective prediction of junction angle in the area under study shows that optimum junction model of Roy (1983) is better applicable for the present study area; the value of exponent (k) may be -0.20 to get better result; prediction with other models shows wide deviation from measured angle; analysis shows that for the smaller angles Horton's model is better predictive and Howard's model is better applicable for the larger angles

Junction Points	09/03/07		02/09/07		26/06/09	
	Actual Angle (ø)	Horton (1932, 1945)	Actual Angle (ø)	Horton (1932, 1945)	Actual Angle (ø)	Horton (1932, 1945)
C <sub>20</sub>	40	64°07'	45	62°44'	55	63°26'
C <sub>21</sub>	35	26°47'	75	61°29'	56	75°47'
C <sub>25</sub>	-	-	-	-	-	-
C <sub>1</sub>	45	71°02'	60	40°03'	35	52°36'
C <sub>2</sub>	52	59°25'	70	34°35'	65	71°02'
C <sub>26</sub>	-	-	-	-	-	-
C <sub>3</sub>	70	68°38'	85	51°22'	75	61°01'
C <sub>4</sub>	60	52°41'	70	47°35'	52	40°35'
I	35	51°30'	69	60°	51	60°29'
G	58	55°41'	47	70°37'	49	60°19'
C <sub>23</sub>	62	75°54'	75	60°	50	56°40'
C <sub>6</sub>	45	54°55'	60	66°25'	45	44°24'
C <sub>7</sub>	40	43°12'	30	39°32'	25	45°50'
C <sub>5</sub>	35	50°40'	55	48°39'	28	46°31'
C <sub>8</sub>	40	81°22'	70	64°24'	55	66°40'
Q	56	63°14'	35	68°39'	50	54°55'
E	45	54°46'	60	51°52'	56	53°15'
C <sub>24</sub>	55	63°33'	40	59°57'	50	56°14'
C <sub>9</sub>	52	48°14'	85	53°48'	55	56°14'
E <sub>1</sub>	70	84°00'	65	70°19'	70	56°22'
C	50	74°22'	60	67°24'	75	33°36'
C <sub>1</sub>	60	46°48'	57	50°55'	50	40°35'
C <sub>10</sub>	45	57°20'	60	51°46'	52	39°59'
K <sub>1</sub>	-	-	45	48°11'	60	54°42'
K	40	37°9'	50	44°33'	42	48°12'
C <sub>22</sub>	46	45°51'	48	51°30'	54	44°33'
V	30	61°1'	56	54°16'	30	54°46'
C <sub>13</sub>	45	58°15'	68	53°01'	65	32°51'
C <sub>19</sub>	70	54°55'	65	56°20'	52	40°32'
C <sub>11</sub>	62	64°17'	68	66°10'	61	57°34'
C <sub>12</sub>	47	50°54'	50	48°39'	42	36°53'
M	32	32°39'	65	69°09'	55	45°51'
T	36	67°46'	50	57°43'	65	60°00'
C <sub>14</sub>	65	33°26'	65	63°30'	56	42°34'
C <sub>15</sub>	52	48°22'	56	51°19'	66	33°35'
X <sub>1</sub>	-	-	42	46°03'	40	38°37'
C <sub>16</sub>	-	-	60	60°19'	50	64°15'
O <sub>2</sub>	55	59°44'	55	48°27'	60	43°12'
C <sub>18</sub>	55	60°16'	50	45°28'	42	38°29'
C <sub>17</sub>	22	21°23'	40	36°20'	30	37°22'

Table 3 (Continue)

12/09/09

Junction Points	Actual Angle (θ)	Horton (1932, 1945) GM	Howard (1971) GM	Howard (1971c) MPLM	Roy (1983) OJM X = 1+K				
					Symmetry ratio	K = -0.15	K = -0.20	K = -0.25	K = -0.4
C <sub>20</sub>	72	65°21'	124°12'	-	0.033	60.78	67.93	73.52	84.85
C <sub>21</sub>	62	57°21'	55°09'	63°41'	0.216	53.85	61.36	67.69	82.38
C <sub>25</sub>	62	-	-	157°11'	0.105	56.30	63.69	69.77	83.28
C <sub>1</sub>	58	58°40'	84°53'	133°39'	0.047	59.38	66.62	74.37	84.38
C <sub>2</sub>	62	62°32'	75°04'	77°11'	0.107	57.85	64.62	69.71	83.25
C <sub>26</sub>	56	-	-	122°56'	0.100	56.48	63.86	69.92	83.33
C <sub>3</sub>	70	70°09'	93°18'	94°58'	0.138	55.43	62.76	68.74	82.93
C <sub>4</sub>	69	37°39'	80°50'	98°35'	0.199	54.12	61.50	67.90	82.47
I	65	39°10'	78°11'	79°15'	0.500	51.85	59.48	66.00	64.38
G	53	33°56'	113°07'	116°40'	0.516	51.90	59.43	65.96	81.62
C <sub>23</sub>	65	29°35'	115°09'	180°56'	0.167	54.67	62.14	68.38	82.68
C <sub>6</sub>	72	49°08'	101°24'	103°56'	0.750	51.43	59.04	65.61	81.48
C <sub>7</sub>	56	16°14'	64°00'	65°21'	0.600	51.65	59.24	73.27	81.55
C <sub>5</sub>	36	33°26'	44°30'	46°29'	0.611	51.62	59.22	65.77	81.53
C <sub>8</sub>	62	48°50'	94°38'	112°29'	0.167	54.67	62.14	68.38	82.68
Q	75	45°35'	100°00'	-	-	-	-	-	-
E	25	50°46'	96°55'	-	0.037	60.33	67.50	73.15	84.70
C <sub>24</sub>	-	-	-	-	-	-	-	-	-
C <sub>9</sub>	75	45°35'	100°00'	100°03'	0.652	51.70	59.15	65.71	81.52
E <sub>1</sub>	55	75°24'	113°39'	114°38'	0.222	53.77	61.28	67.62	82.35
C	75	62°41'	79°57'	80°33'	0.405	52.28	59.84	66.32	81.78
C <sub>1</sub>	45	48°39'	110°42'	126°00'	0.275	53.18	60.71	67.10	82.11
C <sub>10</sub>	65	46°48'	96°18'	103°38'	0.230	53.67	61.18	67.53	82.30
K <sub>1</sub>	-	-	-	-	-	-	-	-	-
K	56	41°35'	108°11'	109°49'	0.484	51.95	59.53	66.05	81.67
C <sub>22</sub>	50	35°25'	89°48'	-	0.060	58.43	65.71	71.57	84.05
V	60	22°11'	84°06'	159°44'	0.130	55.53	62.96	69.11	83.00
C <sub>13</sub>	36	19°19'	81°28'	81°46'	0.751	51.43	59.04	65.61	81.21
C <sub>19</sub>	70	17°51'	115°29'	-	0.249	53.45	61.00	67.33	82.23
C <sub>11</sub>	65	34°04'	119°26'	-	0.250	53.43	60.95	67.32	82.21
C <sub>12</sub>	52	43°24'	116°28'	117°21'	0.605	51.63	59.24	65.78	81.55
M	62	35°21'	125°41'	125°54'	0.714	51.46	59.08	65.64	81.48
T	60	44°47'	114°16'	129°8'	0.293	53.00	60.55	66.96	82.05
C <sub>14</sub>	72	37°39'	91°42'	99°30'	0.489	51.91	59.51	66.03	81.65
C <sub>15</sub>	50	42°21'	122°51'	-	0.047	56.58	66.62	72.37	84.38
X <sub>1</sub>	-	-	-	-	-	-	-	-	-
C <sub>16</sub>	-	-	-	115°02'	-	-	-	-	-
O <sub>2</sub>	50	34°04'	81°16'	81°24'	0.750	51.43	59.04	65.61	81.48
C <sub>18</sub>	55	21°15'	62°30'	63°27'	0.560	51.74	59.32	65.86	81.58
C <sub>17</sub>	48	16°14'	64°00'	-	0.250	53.43	60.95	67.32	82.22

observed by mainly headward growth (Bryan and Poesen, 1989). Bifurcation at source and branching along the valley side maintained the law of Tran's link development that is expected on homogeneous slope and materials. The network development at an interval of one hour were recorded and mapped accordingly to monitor the position and angular value of the confluences. The study showed that lower most junctions like A and C experienced downstream migration at a rate of 0.2-0.5 cm/h (Fig. 7). As the other factors remained constant, the duration of exposure to stress (rainfall) of certain intensity seemed to be important in the variation of network. Through the plot was set at a constant angle (20°), the local variation in the redistribution of materials according to availability

of power was responsible for micro scale difference in the gradient. This distribution pattern also varied with time. The materials once deposited at one confluence, started shifting after attaining critical power and so no confluence showed a constant situation of either erosion or deposition. Thus within constant slope, lithology and rain, local variation in the gradient led to the variation in the distribution of energy (Wirtz *et al.*, 2012). This spatio-temporal variation in energy distribution was responsible for the change in the confluence angle (Torri *et al.*, 2006).

**Prediction of junction angle:** There is an increasing need for predicting drainage network characters, specially the angular component, that regulates the flow

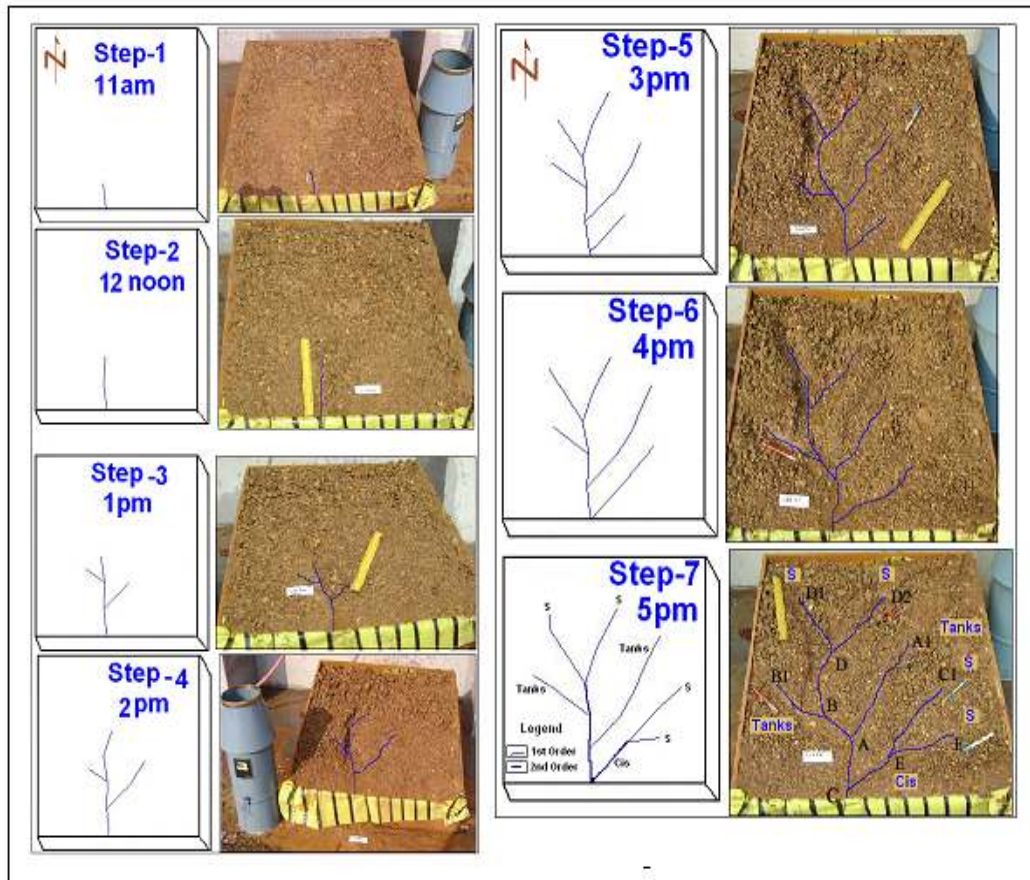


Fig. 7: The plot experiment for monitoring the mechanism of channel development under constant rain on homogeneous gradient and soil; channelization starts after 2 h of sheet wash; branching started after another one and half hours after initiation of channels. Branches are developed from both sides of main channel showing the mode of ‘Trans links’ development due to homogeneous lithology and gradient. Network extends over entire plots in a manner to have equal catchment per unit length of link

Table 4: Plot experiment on a 1 m x 1m plot set at 20° slope gradient, under simulated rain of 16.45 mm/h showed uniform sheet wash for initial 2 h. Since then gradual extension of channels by head ward erosion and branching were observed. In order to adjust with variable situation of either erosion or deposition junction angle changes; confluence points gradually shifts downstream to get adjusted with dynamic discharge and gradient; infiltration rate ranging from 5.8-1.2 mm/h

Period (Time)	Confluence points	Receiving stream			Tributary stream			Junction of angle (deg.)	Down stream migration during 1 h.	
		Name	Length (cm)	Gradient (deg)	Name	Length (cm)	Gradient (deg)			
10- 11am		Sheet wash								
11 12noon		Sheet wash								
12-1 pm	A	AB <sub>2</sub>	21	10	AA <sub>1</sub>	15	12	45		
	B	BB <sub>2</sub>	10.5	11	BB <sub>1</sub>	10	13	54		
1-2 pm	A	AB <sub>2</sub>	31.7	10	AA <sub>1</sub>	25	12	40	1.0 cm	
	B	BB <sub>2</sub>	18.7	11	BB <sub>1</sub>	8.3	13	56		
2-3pm	C	CD <sub>2</sub>	67.48	10	CC <sub>1</sub>	20.8	12	52		
	A	AD <sub>2</sub>	55	12	AA <sub>1</sub>	41.6	14	45	0.5 cm	
	B	BD <sub>2</sub>	42	14	BB <sub>1</sub>	18.72	17	51		
	D	DD <sub>2</sub>	29	15	DD <sub>1</sub>	10	19	56		
3-4 pm	C	CD <sub>2</sub>	71.04	09	CC <sub>1</sub>	41.6	11	42	0.4 cm	
	A	AD <sub>2</sub>	58.56	12	AA <sub>1</sub>	52	13	41	0.5 cm	
	B	BD <sub>2</sub>	44	13	BB <sub>1</sub>	22.88	15	43		
	D	DD <sub>2</sub>	30	16	DD <sub>1</sub>	29.12	18	58	0.3 cm	
4-5pm	C	CD <sub>2</sub>	83	09	CC <sub>1</sub>	60	10	50	0.2 cm	
	A	AD <sub>2</sub>	68	10	AA <sub>1</sub>	62	11	45		
	B	BD <sub>2</sub>	53	13	BB <sub>1</sub>	32	14	50		
	D	DD <sub>2</sub>	38	16	DD <sub>1</sub>	37	17	55		
	E	EC <sub>1</sub>	35	13	EF	15	14	40		

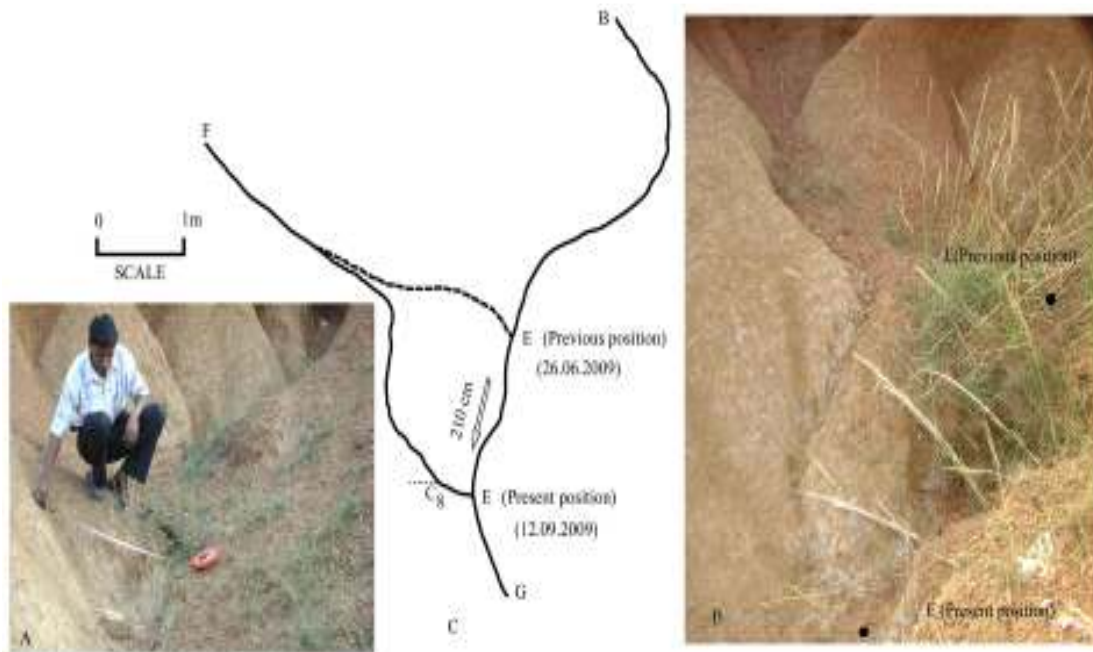


Fig. 8: (a) Earlier junction of EF with parent stream AB as surveyed on 26.06.2009, (b) huge deposits covered the earlier junction E, (c) in response to the catastrophic rain of 12<sup>th</sup> Sept. 2009. A huge deposit was observed at the confluence. Channel was forced to shift right ward, to avoid the deposit. Avulsion of EF thus shifted the confluence downward by 210 cm. Instead of direct contribution to the parent stream AB, EF was observed to join C<sub>8</sub>M<sub>8</sub> on 12.09.2009

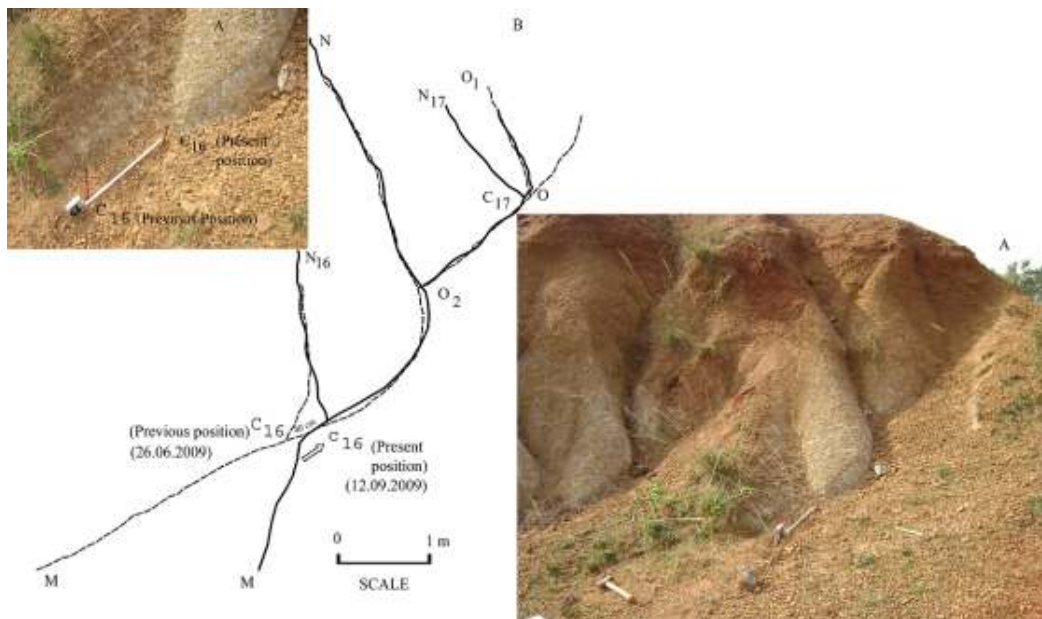


Fig. 9: (a) Huge rain on 12<sup>th</sup> Sept. 2009 capacitates the link C<sub>16</sub> N<sub>6</sub> to straighten its course, (b) the confluence C<sub>16</sub> is shifted upstream by 40 cm in this process of straightening of course

of mass and energy from upper to lower catchment as well as the confluence character (Poesen *et al.*, 2003). Confluence angles largely depend on the gradient and discharge of the tributary and those of the main streams. Following Horton (1945) and Howard (1971) wider angle is related to steeper tributaries where as lower

angle is associated to the incoming links of equal gradient. The confluences with wider angles are more dynamic and susceptible to migration and flooding, where as the confluence with low junction angles are more stable (Roy and Sinha, 2007). The flow characters and morphology of a junction is controlled by the

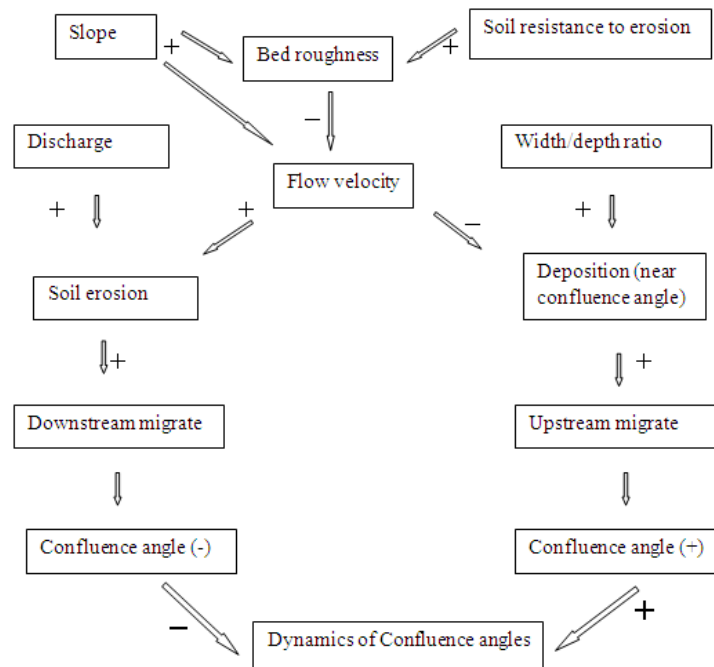


Fig. 10: Conceptual model of the factors influencing Confluence angle in rills or gullies; the increase in gradient leads to greater flow velocity along the links; being assisted with greater discharge, the streams are capacitated with greater power to carry on active erosion at the confluence that leads to lowering of confluence angle and downstream migration; the deposition at confluence, on the other hand, is facilitated by reduction in gradient and resultant reduction in velocity; this favours in increasing confluence angle and associated upstream migration

symmetry ratio, junction angle, gradient of the incoming streams, discharge ratio, zone of flow separation and bank stability (Mosley, 1976; Roy, 1983, 1985; Best, 1988; Bristow *et al.*, 1993; Roy and Sinha, 2007).

The observed data collected on 09-03-2007; 02-09-2007; 26-06-2009 and 12-09-2009 are calibrated to the model proposed by Horton (1945), Howard (1971, 1971c) and Roy (1983) and expected angles are calculated. The analysis of validity of models, efficient to predict junction angles for the present study area shows that optimum junction model Roy (1983) is more valid considering the value of exponent (k) of -0.20. The discharge is considered as the product of a number of hydro-geomorphic factors. The ratio between the discharge of minor ( $Q_2$ ) and major tributary ( $Q_1$ ), the "symmetry ratio" proposed by Roy (1983) is thus taken as an important criteria to determine the confluence angle (Roy, 1983; Best, 1988; Benda, 2008). Roy (1983) experimented his model on large drainage network from Devon and the value of 'k' was estimated to be -0.4 and for the smaller basin, the value of 'k' was proposed to be -0.30 (Roy, 1985). However, in the present study on smaller ephemeral gully basin the values of 'k' become -0.20, (Table 3). Horton (1945) seems to be efficient for the angles of lower value where as Howard (1971) model is efficient to predict those of higher values.

## CONCLUSION

The confluence may be considered as a comprehensive environment rather than a mere junction of links. The temporal variability of influx of sediment and water supply from the tributary basin to the main river essentially affect the environment and that is managed by the internal systematic interaction of rain intensity, gradient, channel width and depth that ultimately lead to either deposition or erosion (Fig. 10). This erosion and deposition changes the junction angles guided by the mechanism of flow separation. The present study reveals that erosion or deposition at the confluence also regulates its migration by changing in junction angles. The dynamic nature of confluence environment is associated to the threshold conditions which are episodic in nature. The change in confluence angles and related shift in the position of junctions associated to some catastrophic rainfall. During the study period (09-03-2007 to 12-09 2009) four catastrophic rains occurred on 7<sup>th</sup> July, 2007, 14<sup>th</sup> August, 2009, 6<sup>th</sup> September, 2009 and 12<sup>th</sup> September, 2009 with rain intensity of 10.53, 12.72, 7.70 and 17.64 mm/h, respectively. Close observation and continuous monitoring of the dynamic nature of drainage links and the confluence angles revealed that all the noticeable changes are occurred during these catastrophic events

being separated by a long period of relative stability. Thus no average rate of change can be proposed.

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